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A unified method for optimal arbitrary pole placement

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Abstract

We consider the classic problem of pole placement by state feedback. We offer an eigenstructure assignment algorithm to obtain a novel parametric form for the pole-placing feedback matrix that can deliver any set of desired closed-loop eigenvalues, with any desired multiplicities. This parametric formula is then exploited to introduce an unconstrained nonlinear optimisation algorithm to obtain a feedback matrix that delivers the desired pole placement with optimal robustness and minimum gain. Lastly we compare the performance of our method against several others from the recent literature.

Key words: linear systems, pole placement, optimal control.

1 Introduction

We consider the classic problem of repeated pole placement for linear time-invariant (LTI) systems in state space form

$$\dot{x}(t) = Ax(t) + Bu(t), \quad (1)$$

where, for all $t \in \mathbb{R}$, $x(t) \in \mathbb{R}^n$ is the state and $u(t) \in \mathbb{R}^m$ is the control input. We assume that B has full column-rank, and that the pair (A, B) is reachable. We let $\mathcal{L} = \{\lambda_1, \dots, \lambda_\nu\}$ be a self-conjugate set of $\nu \leq n$ complex numbers, with associated algebraic multiplicities $\mathcal{M} = \{m_1, \dots, m_\nu\}$ satisfying $m_1 + \dots + m_\nu = n$, and $m_i = m_j$ whenever $\lambda_i = \bar{\lambda}_j$. The problem of *exact pole placement (EPP) by state feedback* is that of finding a real feedback matrix F such that

$$(A + BF)X = X\Lambda, \quad (2)$$

where Λ is a $n \times n$ Jordan matrix obtained from the eigenvalues of \mathcal{L} , including multiplicities given by \mathcal{M} , and X is a matrix of closed-loop eigenvectors of unit length. The

matrix Λ can be expressed in the Jordan (complex) block diagonal canonical form

$$\Lambda = \text{blkdiag}(J(\lambda_1), \dots, J(\lambda_\nu)), \quad (3)$$

where each $J(\lambda_i)$ is a Jordan matrix for λ_i of order m_i , and may be composed of up to g_i mini-blocks

$$J(\lambda_i) = \text{blkdiag}(J_1(\lambda_i), \dots, J_{g_i}(\lambda_i)), \quad (4)$$

where $1 \leq g_i \leq m_i$. We use $\mathcal{P} \stackrel{\text{def}}{=} \{p_{i,k} \mid 1 \leq i \leq \nu, 1 \leq k \leq g_i\}$ to denote the order of each Jordan mini-block $J_k(\lambda_i)$; then $p_{i,k} = p_{j,k}$ whenever $\lambda_i = \bar{\lambda}_j$. When (A, B) is reachable, arbitrary multiplicities of the closed-loop eigenvalues can be assigned by state feedback, but the possible mini-block orders of the Jordan structure of $A + BF$ are constrained by the *controllability indices* (Rosenbrock, 1970). If \mathcal{L} , \mathcal{M} and \mathcal{P} satisfy the conditions of the Rosenbrock theorem, we say that the triple $(\mathcal{L}, \mathcal{M}, \mathcal{P})$ defines an *admissible Jordan structure* for (A, B) .

In order to consider optimal selections for the feedback matrix, it is important to have a parametric formula for the set of feedback matrices that deliver the desired pole placement. In (Kautsky *et al*, 1985) and (Schmid *et al*, 2014) parametric forms are given for the case where Λ is a diagonal matrix and the eigenstructure is non-defective; this requires $m_i \leq m$ for all $m_i \in \mathcal{M}$. Parameterisations that do not impose a con-

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straint on the multiplicity of the eigenvalues to be assigned include (Bhattacharyya and de Souza, 1982) and (Fahmy and O'Reilly, 1983); however these methods require the closed-loop eigenvalues to all be distinct from the open-loop ones.

The general case where \mathcal{L} contains any desired closed-loop eigenvalues and multiplicities is considered in (Chu, 2007) and (Ait Rami *et al.*, 2009), where parametric formulae are provided for F that use the eigenvector matrix X as a parameter. Maximum generality in these parametric formulae has however been achieved at the expense of efficiency, as the square matrix X has n^2 free parameters. By contrast, methods (Kautsky *et al.*, 1985, Fahmy and O'Reilly, 1983, Bhattacharyya and de Souza, 1982, Schmid *et al.*, 2014) all employ parameter matrices with mn free parameters.

The first aim of this paper is to offer a parameterisation for the pole-placing feedback matrix that combines the generality of (Chu, 2007) and (Ait Rami *et al.*, 2009) with the efficiency of an mn -dimensional parameter matrix. We offer a parametric formula for all feedback matrices F solving (2) for any admissible $(\mathcal{L}, \mathcal{M}, \mathcal{P})$. For a given parameter matrix K , we obtain the eigenvector matrix X_K and feedback matrix F_K by building the Jordan chains from eigenvectors selected from the kernels of the matrix pencils $[A - \lambda_i I_n \ B]$, and thus avoid the need for matrix inversions, or the solution of Sylvester matrix equations. The parameterisation will be shown to be exhaustive of all feedback matrices that assign the desired eigenstructure.

The second aim of the paper is to seek the solution to some optimal control problems. We firstly consider the *robust exact pole placement problem* (REPP), which involves obtaining F that renders the eigenvalues of $A + BF$ as insensitive to perturbations in A , B and F as possible. Numerous results (Chatelin, 1993) have appeared linking the sensitivity of the eigenvalues to various measures of the *condition number* of X . Another commonly used robustness measure is the *departure from normality* of the closed loop matrix $A + BF$. For the case of diagonal Λ , there has been considerable literature on the REPP, including (Kautsky *et al.*, 1985, Byers and Nash, 1989, Tits and Yang, 1996, Varga, 2000, Ait Rami *et al.*, 2009, Chu, 2007, Li *et al.*, 2011, Schmid *et al.*, 2014). Papers considering the REPP for the general case where $(\mathcal{L}, \mathcal{M}, \mathcal{P})$ defines an admissible Jordan structure include (Lam *et al.*, 1997) and (Ait Rami *et al.*, 2009).

A related optimal control problem is the *minimum gain exact pole placement problem* (MGEPP), which involves solving the EPP problem and also obtaining the feedback matrix F that has the least gain (smallest matrix norm), which gives a measure of the control amplitude or energy required by the control action. Recent papers addressing the MGEPP with minimum Frobenius norm for F include (Ataei and Enshae, 2011) and (Kochetkov and Utkin, 2014).

In this paper we utilise our parametric form for the matrices X and F that solve (2) to take a unified approach to the REPP and MGEPP problems, for any admissible Jordan structure. In our first method for the REPP, we seek the parameter matrix K that minimises the Frobenius condition number of X . In our second approach to the REPP, we seek

the parameter matrix that minimises the departure from normality of matrix $A + BF$. Next we address the MGEPP by seeking the parameter K that minimises the Frobenius norm of F . Finally, we combine these approaches by introducing an objective function expressed as a weighted sum of robustness and gain measures, and use gradient iterative methods to seek a local minimum.

The performance of the our algorithm will be compared against the methods of (Ait Rami *et al.*, 2009), (Ataei and Enshae, 2011) and (Li *et al.*, 2011) on a number of sample systems. We see that the methods introduced in this paper can achieve superior robustness while using less gain than all three of these alternative methods.

2 Arbitrary pole placement

Here we adapt the algorithm of (Klein and Moore, 1977) to obtain a simple parametric formula for the gain matrix F that solves the exact pole placement problem for an admissible Jordan structure $(\mathcal{L}, \mathcal{M}, \mathcal{P})$, in terms of an arbitrary parameter matrix K with mn free dimensions. We begin with some definitions.

Given a self-conjugate set of v complex numbers $\{\lambda_1, \dots, \lambda_v\}$ containing σ complex conjugate pairs, we say that the set is σ -conformably ordered if the first 2σ values are complex while the remaining are real, and for all odd $i \leq 2\sigma$ we have $\lambda_{i+1} = \bar{\lambda}_i$. For example, the set $\{10j, -10j, 2+2j, 2-2j, 7\}$ is 2-conformably ordered. For simplicity we shall assume in the following that \mathcal{L} is σ -conformably ordered.

If M is a complex matrix partitioned into v column matrices $M = [M_1 \dots M_v]$, we say that M is σ -conformably ordered if the first 2σ column matrices of M are complex while the remaining are real, and for all odd $i \leq 2\sigma$ we have $M_{i+1} = \bar{M}_i$. For a σ -conformably ordered complex matrix M , we define a real matrix $Re(M)$ composed of v column matrices of the same dimensions as those of M thus: for each odd $i \in \{1, \dots, 2\sigma\}$, the i -th and $i+1$ -st column matrices of $Re(M)$ are $\frac{1}{2}(M_i + M_{i+1})$ and $\frac{1}{2j}(M_i - M_{i+1})$ respectively, while for $i \in \{2\sigma + 1, \dots, v\}$, the column matrices of $Re(M)$ are the same as the corresponding column matrices of M . For any real or complex matrix X with $n+m$ rows, we define matrices $\bar{\pi}(X)$ and $\underline{\pi}(X)$ by taking the first n and last m rows of X , respectively. For each $i \in \{1, \dots, v\}$, we define the matrix pencil

$$S(\lambda_i) \stackrel{\text{def}}{=} \begin{bmatrix} A - \lambda_i I_n & B \end{bmatrix}. \quad (5)$$

We use N_i to denote an orthonormal basis matrix for the kernel of $S(\lambda_i)$. If $\lambda_{i+1} = \bar{\lambda}_i$, then $N_{i+1} = \bar{N}_i$. Since each $S(\lambda_i)$ is $n \times (n+m)$ and (A, B) is reachable, each kernel has dimension m . We let

$$M_i \stackrel{\text{def}}{=} \begin{bmatrix} A - \lambda_i I_n & B \end{bmatrix}^\dagger, \quad (6)$$

where \dagger indicates the Moore-Penrose pseudo-inverse. For any matrix X we use $X(l)$ to denote the l -th column of X .

We say that a matrix K is a *compatible parameter matrix* for $(\mathcal{L}, \mathcal{M}, \mathcal{P})$, if $K \stackrel{\text{def}}{=} \text{blkdiag}\{K_1, \dots, K_v\}$, where each K_i has dimension $m \times m_i$, and for each $i \geq 2\sigma$, K_i is a real matrix, and for all odd $i \leq 2\sigma$, we have $K_{i+1} = \overline{K}_i$. Then each K_i matrix may be partitioned as

$$K_i = \begin{bmatrix} K_{i,1} & K_{i,2} & \dots & K_{i,g_i} \end{bmatrix}, \quad (7)$$

where each $K_{i,k}$ has dimension $m \times p_{i,k}$. For $i \in \{1, \dots, v\}$ and $k \in \{1, \dots, g_i\}$ we build vector chains of length $p_{i,k}$ as

$$h_{i,k}(1) = N_i K_{i,k}(1), \quad (8)$$

$$h_{i,k}(2) = M_i \overline{\pi}\{h_{i,k}(1)\} + N_i K_{i,k}(2), \quad (9)$$

\vdots

$$h_{i,k}(p_{i,k}) = M_i \overline{\pi}\{h_{i,k}(p_{i,k}-1)\} + N_i K_{i,k}(p_{i,k}). \quad (10)$$

From these column vectors we construct the matrices

$$H_{i,k} \stackrel{\text{def}}{=} [h_{i,k}(1) \dots h_{i,k}(p_{i,k})] \quad (11)$$

of dimension $(n+m) \times p_{i,k}$, and

$$H_i \stackrel{\text{def}}{=} [H_{i,1} \dots H_{i,g_i}], \quad H_K \stackrel{\text{def}}{=} [H_1 \dots H_v], \quad X_K \stackrel{\text{def}}{=} \overline{\pi}\{H_K\} \quad (12)$$

of dimension $(n+m) \times m_i$, $(n+m) \times n$ and $n \times n$, respectively. Note that H_K is σ -conformably ordered, and hence we may define real matrices

$$V_K \stackrel{\text{def}}{=} \overline{\pi}\{Re(H_K)\}, \quad W_K \stackrel{\text{def}}{=} \underline{\pi}\{Re(H_K)\} \quad (13)$$

of dimensions $n \times n$ and $m \times n$, respectively. We are now ready to present the main result of this paper.

Theorem 2.1 *For almost all choices of the compatible parameter matrix K , the matrix V_K in (13) is invertible. The set of all real feedback matrices F such that $A + BF$ has Jordan structure given by $(\mathcal{L}, \mathcal{M}, \mathcal{P})$ is parameterised in K as*

$$F_K = W_K V_K^{-1}. \quad (14)$$

Proof: Firstly we let K be any compatible parameter matrix yielding invertible V_K and W_K in (13) and F_K in (14). We prove that the closed-loop matrix $A + BF_K$ has the required eigenstructure. V_K and W_K may be partitioned as

$$V_K = [V_1 \dots V_v], \quad W_K = [W_1 \dots W_v], \quad (15)$$

where, for each $i \in \{1, \dots, v\}$, V_i and W_i have m_i columns. Let $H_{i,k}$ in (11) be partitioned as

$$H_{i,k} = \begin{bmatrix} v'_{i,k}(1) & \dots & v'_{i,k}(p_{i,k}) \\ w'_{i,k}(1) & \dots & w'_{i,k}(p_{i,k}) \end{bmatrix}, \quad (16)$$

where, for each $k \in \{1, \dots, g_i\}$, the column vectors satisfy by construction

$$(A - \lambda_i I_n) v'_{i,k}(1) + B w'_{i,k}(1) = 0, \quad (17)$$

$$(A - \lambda_i I_n) v'_{i,k}(2) + B w'_{i,k}(2) = v'_{i,k}(1), \quad (18)$$

\vdots

$$(A - \lambda_i I_n) v'_{i,k}(p_{i,k}) + B w'_{i,k}(p_{i,k}) = v'_{i,k}(p_{i,k}-1). \quad (19)$$

Define for each $i \in \{1, \dots, v\}$ and $k \in \{1, \dots, g_i\}$,

$$V'_{i,k} = [v'_{i,k}(1) \dots v'_{i,k}(p_{i,k})], \quad W'_{i,k} = [w'_{i,k}(1) \dots w'_{i,k}(p_{i,k})], \quad (20)$$

and next define, for each $i \in \{1, \dots, v\}$, $V'_i = [V'_{i,1} \dots V'_{i,g_i}]$ and $W'_i = [W'_{i,1} \dots W'_{i,g_i}]$. As K is a compatible parameter matrix, we have, for all odd $i \in \{1, \dots, 2\sigma\}$, $V'_{i+1} = \overline{V}'_i$ and $W'_{i+1} = \overline{W}'_i$. Finally, introduce $U_i \stackrel{\text{def}}{=} \frac{1}{2} \begin{bmatrix} I_{m_i} & -jI_{m_i} \\ I_{m_i} & jI_{m_i} \end{bmatrix}$.

Then for each odd $i \in \{1, \dots, 2\sigma\}$, we have $[V'_i \ V'_{i+1}] U_i = [V_i \ V_{i+1}]$ and $[W'_i \ W'_{i+1}] U_i = [W_i \ W_{i+1}]$, and for each $i \in \{2\sigma+1, \dots, v\}$, we have $V'_i = V_i$ and $W'_i = W_i$. Since $F_K V_K = W_K$, then $F_K [V'_i \ V'_{i+1}] = [W'_i \ W'_{i+1}]$ for all odd $i \in \{1, \dots, 2\sigma\}$ and $F_K V_i = W_i$ for all $i \in \{2\sigma+1, \dots, v\}$. Hence, for each odd $i \in \{1, \dots, 2\sigma\}$, we have

$$(A + BF_K) [V'_i \ V'_{i+1}] = [V'_i \ V'_{i+1}] \text{diag}\{J(\lambda_i), J(\lambda_{i+1})\}, \quad (21)$$

and for all $i \in \{2\sigma+1, \dots, v\}$, we have $(A + BF_K) V_i = V_i J(\lambda_i)$. Thus $(A + BF_K) X_K = X_K \Lambda$, where $X_K = [V'_1 \dots V'_v]$ and Λ is as in (3), as required.

In order to prove that the parameterisation is exhaustive, we consider a feedback matrix F such that the eigenstructure of $A + BF$ is given by $(\mathcal{L}, \mathcal{M}, \mathcal{P})$, and show there exists a compatible parameter matrix K such that matrices V_K and W_K can be constructed in (13), with V_K invertible and $F = W_K V_K^{-1}$. From (3)-(4), Λ can be written as

$$\Lambda = \text{blkdiag}(J_1(\lambda_1), \dots, J_{g_1}(\lambda_1), \dots, J_1(\lambda_v), \dots, J_{g_v}(\lambda_v)).$$

Hence there exists an invertible matrix T satisfying $(A + BF)T = T\Lambda$. Let us partition X and Y conformably with the corresponding Jordan mini-blocks that they multiply, i.e.,

$$\begin{bmatrix} A & B \end{bmatrix} \begin{bmatrix} X_{1,1} & \dots & X_{v,g_v} \\ Y_{1,1} & \dots & Y_{v,g_v} \end{bmatrix} = \begin{bmatrix} X_{1,1} J_1(\lambda_1) & \dots & X_{v,g_v} J_{g_v}(\lambda_v) \end{bmatrix}.$$

For $i \in \{1, \dots, v\}$ and $k \in \{1, \dots, g_i\}$, the generic term is

$$\begin{bmatrix} A & B \end{bmatrix} \begin{bmatrix} X_{i,k} \\ Y_{i,k} \end{bmatrix} = X_{i,k} J_k(\lambda_i). \quad (22)$$

First consider the case in which λ_i is real. Partitioning $X_{i,k} = [v_{i,k}(1) \dots v_{i,k}(p_{i,k})]$ and $Y_{i,k} = [w_{i,k}(1) \dots w_{i,k}(p_{i,k})]$, we

can write (22) as

$$\begin{bmatrix} A & B \end{bmatrix} \begin{bmatrix} v_{i,k}(1) \dots v_{i,k}(p_{i,k}) \\ w_{i,k}(1) \dots w_{i,k}(p_{i,k}) \end{bmatrix} = \begin{bmatrix} v_{i,k}(1) \dots v_{i,k}(p_{i,k}) \\ w_{i,k}(1) \dots w_{i,k}(p_{i,k}) \end{bmatrix} J_k(\lambda_i),$$

which yields

$$A v_{i,k}(1) + B w_{i,k}(1) = v_{i,k}(1) \lambda_i \quad (23)$$

$$A v_{i,k}(2) + B w_{i,k}(2) = v_{i,k}(1) + \lambda_i v_{i,k}(2) \quad (24)$$

\vdots

$$A v_{i,k}(p_{i,k}) + B w_{i,k}(p_{i,k}) = v_{i,k}(p_{i,k} - 1) + \lambda_i v_{i,k}(p_{i,k}) \quad (25)$$

We denote $h_{i,k}(l) = \begin{bmatrix} v_{i,k}(l) \\ w_{i,k}(l) \end{bmatrix}$. From (23) we see that $h_{i,k}(1) \in \ker(S(\lambda_i))$ and hence there exists $K_{i,k}(1)$ satisfying (8). Moreover, from (24) we find $[A - \lambda_i I_n \ B] h_{i,k}(2) = v_{i,k}(1)$, which implies that there exists $K_{i,k}(2)$ satisfying (9). Repeating this procedure for all $l \in \{1, \dots, p_{i,k}\}$, we find the parameters $K_{i,k}(1), \dots, K_{i,k}(p_{i,k})$ which satisfy (8)-(10). This procedure can be carried out for all real Jordan mini-blocks. Consider now the case of a real mini-block associated with a complex conjugate eigenvalue $\lambda_i = \sigma_i + j \omega_i$. For brevity we shall assume $p_{i,k} = 2$. Thus, (23) becomes

$$\begin{bmatrix} A & B \end{bmatrix} \begin{bmatrix} v_{i,k}(1) & v_{i,k}(2) & v_{i+1,k}(1) & v_{i+1,k}(2) \\ w_{i,k}(1) & w_{i,k}(2) & w_{i+1,k}(1) & w_{i+1,k}(2) \end{bmatrix} = \begin{bmatrix} v_{i,k}(1) & v_{i,k}(2) & v_{i+1,k}(1) & v_{i+1,k}(2) \end{bmatrix} \begin{bmatrix} \sigma_i & \omega_i & 1 & 0 \\ -\omega_i & \sigma_i & 0 & 1 \\ 0 & 0 & \sigma_i & \omega_i \\ 0 & 0 & -\omega_i & \sigma_i \end{bmatrix},$$

which can be re-written as

$$\begin{bmatrix} A & B \end{bmatrix} \begin{bmatrix} v_{i,k}(1) + j v_{i,k}(2) & v_{i+1,k}(1) + j v_{i+1,k}(2) \\ w_{i,k}(1) + j w_{i,k}(2) & w_{i+1,k}(1) + j w_{i+1,k}(2) \end{bmatrix} = \begin{bmatrix} v_{i,k}(1) + j v_{i,k}(2) & v_{i+1,k}(1) + j v_{i+1,k}(2) \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \sigma_i + j \omega_i & 1 \\ 0 & \sigma_i + j \omega_i \end{bmatrix},$$

and the arguments above can be utilised after a re-labeling of the vectors.

Lastly we show that V_K is invertible for almost all choices of the parameter matrix K . For each $i \in \{1, \dots, \nu\}$, we may express the orthonormal basis N_i for $\ker(S(\lambda_i))$ as $N_i = [h_{i,1} \dots h_{i,m}]$. For each $k \in \{1, \dots, g_i\}$ we construct

$$h_{i,k}(1) = h_{i,k} \quad (26)$$

$$h_{i,k}(2) = M_i h_{i,k}(1) \quad (27)$$

\vdots

$$h_{i,k}(p_{i,k}) = M_i h_{i,k}(p_{i,k} - 1) \quad (28)$$

and combining these we obtain

$$H_{i,k} = [h_{i,k}(1) \dots h_{i,k}(p_{i,k})]. \quad (29)$$

Lastly we obtain matrices H_i and H as in (12), and V as in (13). Then we must have $\text{rank}(V) = n$, else no parameter matrix K would exist to yield a real feedback matrix F_K in (14) that delivers the desired closed-loop eigenstructure. This contradicts the assumption that (A, B) is reachable.

Next let K be any compatible parameter matrix for $(\mathcal{L}, \mathcal{M}, \mathcal{P})$, let $V_K = \bar{\pi}\{\text{Re}(H_K)\}$ and assume V_K is singular. Then X_K in (12) is also singular, i.e. $\text{rank}(X_K) \leq n - 1$. Without loss of generality, assume the first column of X_K is linearly dependent upon the remaining ones. Then there exist a σ -conformalby ordered set of n coefficient vectors $\alpha_{i,k,l}$, not all equal to zero, for which

$$\begin{aligned} \bar{\pi}\{h_{1,1}(1)K_{1,1}(1)\} &= \sum_{l=2}^{p_{1,1}} \alpha_{1,1,l} \bar{\pi}\{h_{1,1}(l)\} \\ &+ \sum_{k=2}^{g_1} \sum_{l=1}^{p_{1,k}} \alpha_{1,k,l} \bar{\pi}\{h_{1,k}(l)\} \\ &+ \sum_{i=2}^{\nu} \sum_{k=1}^{g_i} \sum_{l=1}^{p_{i,k}} \alpha_{i,k,l} \bar{\pi}\{h_{i,k}(l)\} \end{aligned}$$

This implies that $\text{rank}(X_K) = n$ may fail only when $K_{1,1}(1)$ lies on an $(m - 1)$ -dimensional hyperplane in the m -dimensional parameter space. Thus the set of compatible parameter matrices K that can lead to a loss of rank in X_K , and hence V_K , is given by the union of at most n hyperplanes of dimension at most $nm - 1$ in the nm -dimensional parameter space. Since hyperplanes have zero Lebesgue measure, the set of parameter matrices K leading to singular V_K has zero Lebesgue measure. \blacksquare

The above formulation takes its inspiration from the proof of Proposition 1 in (Klein and Moore, 1977), and hence we shall refer to (14) as the *Klein-Moore parametric form* for F .

3 Optimal pole placement methods

We firstly present some classic results on eigenvalue sensitivity. Let A and X be such that $A = XJX^{-1}$, where J is the Jordan form of A , and let $A' = A + H$. Then, for each eigenvalue λ' of A' , there exists an eigenvalue λ of A such that

$$\frac{|\lambda - \lambda'|}{(1 + |\lambda - \lambda'|)^{l-1}} \leq \kappa_2(X) \|H\|_2, \quad (30)$$

where l is the size of the largest Jordan mini-block associated with λ , and $\kappa_2(X) \stackrel{\text{def}}{=} \|X\|_2 \|X^{-1}\|_2$ is the spectral condition number of X (Chatelin, 1993). As the Frobenius condition number $\kappa_{\text{FRO}}(X) = \|X\|_{\text{FRO}} \|X^{-1}\|_{\text{FRO}}$ satisfies $\kappa_2(X) \leq \kappa_{\text{FRO}}(X)$ and is differentiable, it is often used as a robustness measure in conjunction with gradient search methods.

A second widely used robustness measure is the *departure from normality* of the matrix A , which is defined as follows

(Stewart and Sun, 1990): Let U be any unitary matrix such that $U^T A U$ is upper triangular, then $U^T A U = D + R$, for some diagonal matrix D and strictly upper triangular matrix R . The Frobenius departure from normality of A is then $\delta_{\text{FRO}}(A) \stackrel{\text{def}}{=} \|R\|_{\text{FRO}}$.

Our Method 1 simultaneously addresses the REPP and MGEPP by using the weighted objective function

$$f(K) = \alpha \kappa_{\text{FRO}}(V_K) + (1 - \alpha) \|F_K\|_{\text{FRO}}, \quad (31)$$

where K is a compatible parameter matrix and V_K and F_K are obtained from (13) and (14). Finding K to minimise f presents an unconstrained nonconvex optimisation problem. For efficient computation (Byers and Nash, 1989), showed we can use the equivalent objective function

$$f_1(K) = \alpha (\|V_K\|_{\text{FRO}}^2 + \|V_K^{-1}\|_{\text{FRO}}^2) + (1 - \alpha) \|F_K\|_{\text{FRO}}^2, \quad (32)$$

Here, α is a weighting factor, with $0 \leq \alpha \leq 1$. The limiting cases $\alpha = 0$ and $\alpha = 1$ define the MGEPP and REPP problems, respectively.

Our Method 2 uses the weighted objective function

$$f_2(K) = \alpha \delta_{\text{FRO}}^2(A + B F_K) + (1 - \alpha) \|F_K\|_{\text{FRO}}^2. \quad (33)$$

Finding K to minimise f_2 again presents an unconstrained nonconvex optimisation problem. Expressions for the derivatives of H_K , $\|V_K\|_{\text{FRO}}$, and $\|V_K^{-1}\|_{\text{FRO}}$ were given in Schmid *et al* (2013b); from these, gradient search methods can be used to seek local minima for f_1 and f_2 . The results are contingent upon the initial choice of the parameter matrix K .

4 Performance comparisons

In this section, we compare the performance of our algorithm with the methods given in the recent papers by (Ait Rami *et al*, 2009), (Ataei and Enshaeae, 2011) and (Li *et al*, 2011). In (Byers and Nash, 1989) a collection of benchmark systems were introduced that have been investigated over the years by many authors. To compare our performance against the method of (Ait Rami *et al*, 2009), we used the matrices (A, B) from these examples, but in order to compare their performance for defective pole assignment, we assigned all the closed-loop eigenvalues to zero. In each case we assigned Jordan blocks of sizes equal to the controllability indices. Using the toolbox *rfbt* to implement the method of (Ait Rami *et al*, 2009) that we created for our earlier computational survey in (Schmid *et al*, 2014), we obtained the matrices F and X delivered by this method, for each of the 11 sample systems. We also implemented our own method on these systems. The results are shown in Table 1.

Comparing the robust conditioning performance of the two methods, we see little difference between the methods. However, when we compare the matrix gain used to achieve this eigenstructure we observe that our method was able to use less gain in 5 of the sample systems, and in two cases (System 2 and 5) the reduction in gain was very considerable. The results are in agreement with the findings of the survey

Table 1
Byers and Nash examples

Example	Ait Rami <i>et al</i>		Our Method	
	$\kappa_{\text{FRO}}(X)$	$\ F\ _{\text{FRO}}$	$\kappa_{\text{FRO}}(X)$	$\ F\ _{\text{FRO}}$
1	16.73	3.102	16.73	3.102
2	54.43	645.5	51.11	289.5
3	7.188	2.225	7.188	2.225
4	11.49	7.145	11.49	7.043
5	29.99	186.8	28.39	138.0
6	113.4	8.167	113.4	7.880
7	16.84	595.9	17.33	596.1
8	4.000	10.07	4.000	9.230
9	85.68	22,610	85.65	22,610
10	30.33	29.74	30.33	29.74
11	4,579	5,025	4,501	5,025

in (Schmid *et al*, 2014), which considered sample systems with non-defective eigenstructure and found that our method could achieve comparable robust conditioning with that of Ait Rami *et al* (2009), but with reduced gain.

To compare our performance against that of (Ataei and Enshaeae, 2011), we considered the 5 example systems introduced in that paper. Among these, the first example system assigned all the poles to zero, and hence requires a defective closed-loop eigenstructure. The other four sample systems all involve distinct eigenvalues. The results are shown in Table 2. The results have been constructed using the feedback matrices provided by (Ataei and Enshaeae, 2011).

Table 2
Ataei and Enshaeae examples

Example	Ataei and Enshaeae		Our Method	
	$\kappa_{\text{FRO}}(X)$	$\ F\ _{\text{FRO}}$	$\kappa_{\text{FRO}}(X)$	$\ F\ _{\text{FRO}}$
1	321.4	1.295	4.444	1.295
2	290.5	3.970	278.6	3.844
3	7.895	1.311	6.515	1.304
4	3.873	4.243	4.353	4.072
5	26.01	4.748	21.56	4.662

The results show that our method achieved the desired eigenstructure with equal or slightly less gain than that of (Ataei and Enshaeae, 2011). In all but one of the samples, our method also achieved a more robust eigenstructure, especially in Example 1, which has the defective eigenstructure.

Lastly, we consider Example 1 in (Li *et al*, 2011). The four desired closed loop poles are all distinct in this example. The method of (Li *et al*, 2011) considers the problem of minimising the Frobenius norm of the feedback matrix and the minimisation of the departure from normality measure. The authors obtained a feedback F yielding $\delta_{\text{FRO}}(A + B F) = 20.67$, and an alternative matrix F that delivers the desired pole placement with gain $\|F\|_{\text{FRO}} = 6.049$.

Applying Method 2 with $\alpha = 1$ we obtained a feedback matrix F yielding $\delta_{\text{FRO}}(A + B F) = 18.52$, and by using $\alpha = 0$, we obtained F such that $\|F\|_{\text{FRO}} = 3.826$, indicating that our method can achieve the desired pole placement with

either smaller departure from normality measure, or less gain, than the method of (Li *et al*, 2011), as required.

5 Conclusion

We have introduced a novel parametric form for the feedback matrix that solves the classic problem of exact pole placement with any desired eigenstructure. The parametric form was used to take a unified approach to a variety of optimal pole placement problems. The effectiveness of the method has been compared against several recent alternative methods from the literature, and was shown in several examples to achieve the desired pole placement with either superior robustness or smaller gain than the other methods surveyed.

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