Arbitrary pole placement with the extended Kautsky-Nichols-van Dooren parametric form with minimum gain

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Abstract—We consider the classic problem of pole placement by state feedback. We revisit the well-known eigenstructure assignment algorithm of Kautsky, Nichols and van Dooren [1] and extend it to obtain a novel parametric form for the pole-placing feedback matrix that can deliver any set of desired closed-loop eigenvalues, with any desired multiplicities. This parametric formula is then employed to introduce an unconstrained nonlinear optimisation algorithm to obtain a feedback matrix that delivers the desired pole placement with minimum gain.

I. Introduction

We consider the classic problem of repeated pole placement for linear time-invariant (LTI) systems in state space form

$$\dot{x}(t) = Ax(t) + Bu(t), \tag{1}$$

where, for all $t \in \mathbb{R}$, $x(t) \in \mathbb{R}^n$ is the state and $u(t) \in \mathbb{R}^m$ is the control input, and A and B are appropriate dimensional constant matrices. We assume that B has full column-rank, and that the pair (A,B) is reachable. We let $\mathcal{L} = \{\lambda_1,\ldots,\lambda_v\}$ be a self-conjugate set of $v \leq n$ complex numbers, with associated algebraic multiplicities $\mathcal{M} = \{m_1,\ldots,m_v\}$ satisfying $m_1 + \cdots + m_v = n$. The problem of arbitrary *exact pole placement (EPP) by state feedback* is that of finding a real gain matrix F such that the closed-loop matrix A + BF has eigenvalues given by the set \mathcal{L} with multiplicities given by \mathcal{M} , i.e., F satisfies the equation

$$(A + BF)X = X\Lambda, \tag{2}$$

where Λ is a $n \times n$ Jordan matrix obtained from the eigenvalues of \mathcal{L} , including multiplicities, and X is a matrix of closed-loop eigenvectors of unit length. The matrix Λ can be expressed in the Jordan (complex) canonical form

$$\Lambda = \text{blkdiag}\{J(\lambda_1), J(\lambda_2), \cdots, J(\lambda_{\nu})\}$$
 (3)

where each $J(\lambda_i)$ is a Jordan matrix for λ_i of order m_i , and may be composed of g_i mini-blocks

$$J(\lambda_i) = \text{blkdiag}\{J_1(\lambda_i), J_2(\lambda_i), \cdots, J_{e_i}(\lambda_i)\}$$
 (4)

where $g_i \le m$. We use $\mathscr{P} \stackrel{\text{def}}{=} \{p_{i,k} | 1 \le i \le v, 1 \le k \le g_i\}$ to denote the orders of the Jordan mini-blocks $J_k(\lambda_i)$ that comprise $J(\lambda_i)$. It is well-known that when (A,B) is a reachable pair,

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arbitrary multiplicities of the closed-loop eigenvalues can be assigned by state feedback, but the possible orders of the associated Jordan structures are constrained by the system controllability indices (or Kronecker invariants) [2]. If \mathcal{L} , \mathcal{M} and \mathcal{P} satisfy the conditions of the Rosenbrock theorem, we say that the triple $(\mathcal{L}, \mathcal{M}, \mathcal{P})$ defines an admissible Jordan structure for (A, B).

In order to consider optimal selections for the gain matrix, it is important to have a parametric formula for the set of gain matrices that deliver the desired pole placement, and numerous such parameterisations have appeared in the literature over the past three decades. In [1], a method for obtaining suitable F was introduced involving a QR-factorisation for B and a Sylvester equation for X, which requires Λ in (2) to be a diagonal matrix. In particular this means that the desired multiplicities must satisfy $m_i \leq m$ for all $i \in \{1, \ldots, v\}$. Both the widely-used MATLAB® routine place.m and the MATHEMATICA® routine KNVD are based on the algorithm proposed in [1]. In [3] this method was used to develop a parametric formula for X and F, in terms of a suitable parameter matrix; we discuss this method in detail in Section II.

Other parameterisations have been presented in the literature that do not impose a constraint on the multiplicity of the eigenvalues to be assigned. In [4] a procedure was given for obtaining the gain matrix by solving a Sylvester equation in terms of an $n \times m$ parameter matrix, provided the closed-loop eigenvalues do not coincide with the open-loop ones. In [5] a parametric form is presented in terms of the inverses of the matrices $A - \lambda_i I_n$ (where I_n denotes the $n \times n$ identity matrix), which also requires the assumption that the closedloop eigenvalues are all distinct from the open-loop ones. More recently, in [6] the parametric formula of [1] was revisited for the case where Λ was any admissible Jordan matrix, and a parameterisation was obtained for the pole placing matrix F by using the eigenvector matrix X as a parameter. The case where $\mathscr L$ contains any desired closedloop eigenvalues and multiplicities is also considered in [7], where a parametric form for F is presented in terms of the solution to a Sylvester equation, also using the eigenvector matrix X as a parameter. However, maximum generality in these parametric formulae has been achieved at the expense of efficiency. Where methods [1], [4], [5] all employ parameter matrices of dimension $m \times n$, the parameter matrices in

In our recent papers [8]-[9], we gave a novel parametric form for X and F based on the famous pole placement algorithm of Moore [10]. This parameterisation employed parameter

[6] and [7] have dimension $n \times n$.

matrices of dimension $m \times n$, but required Λ to be diagonal, and hence also assumes the closed-loop eigenvalues have multiplicities of at most m. Very recently in our papers [11]-[12] we generalized this parametric form to accommodate arbitrary multiplicities; the method was based on the pole placement method of Klein and Moore [13]. The principal merit of this approach was to obtain a parameterisation that combines the generality of [6] and [7] with the computational efficiency that comes from an $m \times n$ dimensional parameter matrix.

The first aim of this paper is to revisit the pole-placing feed-back method of [1] and generalise it to obtain a parametric formula that can assign arbitrary pole-placement. For a suitable real or complex $m \times n$ parameter matrix K, we obtain the eigenvector matrix X(K) and gain matrix F(K) by building the Jordan chains starting from the selection of eigenvectors from the kernel of certain matrix pencils, and thus avoid the need for matrix inversions, or the solution of Sylvester matrix equations. Thus the results of this paper neatly parallel the achievements of [11] in providing a new parametric form to achieve pole placement with arbitrary multiplicities, while employing an $m \times n$ -dimensional parameter matrix.

The second aim of the paper is to employ this novel parametric form to seek the solution to the *minimum gain exact* pole placement problem (MGEPP), which involves solving the EPP problem and also obtaining the feedback matrix F that has the smallest gain, which is of as a measure of the control amplitude or energy required. In [14] the MGEPP problem is addressed for the specific case of placing multiple deadbeat modes with minimum Frobenius gain. Recently the general problem of assigning any desired set of poles with any desired multiplicities with minimum Frobenius gain has been considered in [15].

Finally, we demonstrate the performance of the resulting algorithm by considering an example involving the assignment of deadbeat modes, and compare the performance against the methods of [11], [14], [15]. We see that the methods introduced in this paper are able to deliver the desired eigenstructure with equivalent or smaller gain than these alternative methods.

We begin with some definitions and notation. We say that \mathcal{L} is σ -conformably ordered if there an integer σ such that the first 2σ values of \mathcal{L} are complex while the remaining are real, and for all odd $k \leq 2\sigma$ we have $\lambda_{k+1} = \overline{\lambda}_k$. For example, the set $\mathcal{L} = \{10j, -10j, 2+2j, 2-2j, 7\}$ is 2-conformably ordered. Notice that, since \mathcal{L} is symmetric, we have $m_i = m_{i+1}$ for odd $i \leq \sigma$. In the following we implicitly assume that an admissible Jordan structure $(\mathcal{L}, \mathcal{M}, \mathcal{P})$ is σ -conformably ordered, for some integer σ . For any matrix X we use X(l) to denote the l-th column of X. The symbol 0_n represents the zero vector of length n, and I_n is the n-dimensional identity matrix.

Let X denote any complex matrix partitioned into submatrices $X = [X_1 ... X_v]$ ordered such that any complex submatrices occur consecutively in complex conjugate pairs, and so that, for some integer s, the first 2s submatrices are complex while the remaining are real. We define a real matrix

 $\mathfrak{Re}\{X\}$ of the same dimension as X thus: if X_i and X_{i+1} are consecutive complex conjugate submatrices of X, then the corresponding submatrices of $\mathfrak{Re}\{X\}$ are $\frac{1}{2}(X_i + X_{i+1})$ and $\frac{1}{2i}(X_i - X_{i+1})$.

II. POLE PLACEMENT METHODS

We now revisit the algorithm of [1] for the gain matrix F that solves the exact pole placement problem (2), for the case where Λ is a diagonal matrix.

Theorem 2.1: ([1], Theorem 3) Given $\Lambda = \text{diag}\{\lambda_1, \lambda_2, \dots, \lambda_n\}$ and X non-singular, then there exists F, a solution to (2) if and only if

$$U_1^{\top} (AX - X\Lambda) = 0, \tag{5}$$

where

$$B = \begin{bmatrix} U_0 & U_1 \end{bmatrix} \begin{bmatrix} Z \\ 0 \end{bmatrix} \tag{6}$$

with $U = [U_0 \ U_1]$ orthogonal and Z nonsingular. Then F is given by

$$F = Z^{-1} U_0^{\top} (X \Lambda X^{-1} - A)$$
 (7)

Corollary 2.1: ([1], Corollary 1) The eigenvector x_i of A + BF corresponding to the assigned eigenvalue $\lambda_i \in \mathcal{L}$ must belong to the space

$$\mathscr{S}_i \stackrel{\text{def}}{=} \ker[U_1^\top (A - \lambda_i I_n)], \tag{8}$$

the null-space of $U_1^{\top}(A - \lambda_i I_n)$.

We note that (6) uses a QR factorisation for B; Byers and Nash [3] pointed out that F may also be obtained from the singular value decomposition for B. Given $B = USG^{\top}$, we let $U = \begin{bmatrix} U_0 & U_1 \end{bmatrix}$ and $SG^{\top} = \begin{bmatrix} Z \\ 0 \end{bmatrix}$. They used Corollary 2.1 to obtain a parametric form for the matrix of eigenvectors X satisfying (2) as follows:

Theorem 2.2: ([3]) Assume the eigenvalues in \mathcal{L} are such that Λ in (2) is a diagonal matrix. Let Σ_i be a $n \times m$ basis matrix for \mathcal{L}_i . Let $\zeta_{(m-1)i+1}, \ldots, \zeta_{mi}$ be the coordinates of the eigenvector x_i with respect to Σ_i . The eigenvector x_i may be written as

$$x_i = \Sigma_i \Xi_i, \quad \Xi_i = [\zeta_{(m-1)i+1}, \dots, \zeta_{mi}] \tag{9}$$

and the eigenvector matrix X is expressible as

$$X = X(\zeta_1, \dots, \zeta_{nm}) = \Sigma \Xi = [\Sigma_1 \dots \Sigma_n] \operatorname{diag} \{\Xi_1, \dots, \Xi_n\},$$
(10)

where diag $\{\Xi_1, \ldots, \Xi_n\}$ is an $nm \times n$ block diagonal matrix with $m \times 1$ blocks, so ζ gives a parameterisation of X and also of F.

Theorem 2.2 assumes real eigenvalues; see Section 2.2 of [3] for a comment on how to accommodate complex eigenvalues. Our aim in this paper is to generalise the parametric form for X and F given in Theorem 2.2 to accommodate any admissible Jordan structure $(\mathcal{L},\mathcal{M},\mathcal{P})$ for (A,B). Our treatment will explicitly accommodate complex eigenvalues. We begin by noting that for each $i \in \{1,\ldots,v\}$, each \mathcal{L}_i has n rows and n+m columns, and as the pair (A,B) is reachable, the dimension of \mathcal{L}_i is equal to m. For each $i \in \{1,2,\ldots,v\}$, we compute maximal rank matrices N_i and M_i satisfying

$$U_1^{\top}(A - \lambda_i I_n) N_i = 0, \quad U_1^{\top}(A - \lambda_i I_n) M_i = I_{n-m}.$$
 (11)

Then N_i is a basis matrix for \mathscr{S}_i . It follows that, for each odd $i \le 2\sigma$, we have $N_{i+1} = \overline{N}_i$ because if $\lambda_{i+1} = \overline{\lambda}_i$.

For any σ -conformably ordered admissible Jordan structure $(\mathcal{L},\mathcal{M},\mathcal{P})$, we say that an $m \times n$ parameter matrix $K \stackrel{\text{def}}{=} \operatorname{diag}\{K_1,\ldots,K_V\}$ is *compatible* with $(\mathcal{L},\mathcal{M},\mathcal{P})$ if: (i) for each $1 \leq i \leq v$, K_i is a matrix of dimension $m \times m_i$; (ii) for all $1 \leq i \leq 2\sigma$, K_i is a complex matrix such that $K_i = \overline{K}_{i+1}$, for all odd $i \leq 2\sigma$, and K_i is a real matrix for each $i \geq 2\sigma$; and (iii) each K_i matrix can be partitioned as

$$K_i = \left[\begin{array}{c|c} K_{i,1} & K_{i,2} & \dots & K_{i,g_i} \end{array} \right], \tag{12}$$

where, for $1 \leq k \leq g_i$, each $K_{i,k}$ has dimension $m \times p_{i,k}$. In this section we develop our parametric form for the eigenvector matrix X and pole-placing gain matrix F that solve (2) for any admissible eigenstructure $(\mathcal{L}, \mathcal{M}, \mathcal{P})$. Our first task is to obtain a suitable eigenvector matrix. Given a compatible $m \times n$ parameter matrix K for $(\mathcal{L}, \mathcal{M}, \mathcal{P})$, we build eigenvector chains as follows. For each pair $i \in \{1, \dots, v\}$ and $k \in \{1, \dots, g_i\}$, build vector chains of length $p_{i,k}$ as follows:

$$x_{i,k}(1) = N_i K_{i,k}(1), (13)$$

$$x_{i,k}(2) = M_i U_1^{\top} x_{i,k}(1) + N_i K_{i,k}(2),$$
 (14)

:

$$x_{i,k}(p_{i,k}) = M_i U_1^{\top} x_{i,k}(p_{i,k} - 1) + N_i K_{i,k}(p_{i,k}).$$
 (15)

From these column vectors we construct the matrices

$$X_{i,k} \stackrel{\text{def}}{=} [x_{i,k}(1)|x_{i,k}(2)|\dots|x_{i,k}(p_{i,k})]$$
 (16)

$$X_i \stackrel{\text{def}}{=} [X_{i,1}|X_{i,2}|\dots|X_{i,g_i}] \tag{17}$$

$$X_K \stackrel{\text{def}}{=} [X_1 | X_2 | \dots | X_V] \tag{18}$$

of dimensions $n \times p_{i,k}$, $n \times m_i$ and $n \times n$, respectively. Finally we obtain the feedback gain matrix

$$F_K \stackrel{\text{def}}{=} Z^{-1} U_0^\top (X_K \Lambda X_K^{-1} - A) \tag{19}$$

Given the origins of this method in the classic paper [1], we shall refer to the parametric formulae (18)-(19) as the extended Kautsky-Nichols-van Dooren parametric form for X and F. We are now ready to present the main result of this paper.

Theorem 2.3: Let $(\mathcal{L}, \mathcal{M}, \mathcal{P})$ be an admissible Jordan structure for (A,B) and let K be a compatible parameter matrix. Then for almost all choices of K, the matrix X_K in (18) is invertible, i.e., X_K is invertible for every choice of K except those lying in a set of measure zero. The set of all real feedback matrices F_K such that the closed-loop matrix $A + BF_K$ has Jordan structure given by $(\mathcal{L}, \mathcal{M}, \mathcal{P})$ is parameterised in K by (19), where X_K is obtained with a parameter matrix K such that K_K is invertible.

Proof: The proof will be carried out in three steps. First, we show that if X_K and F_K are given by (18) and (19) respectively, then (2) is satisfied, provided X_K is invertible. Second, we show that the parametrisation given in (19) is exhaustive, i.e., for every feedback matrix F_K and nonsingular eigenvector matrix X_K satisfying (2), there exists a

compatible parameter matrix K such that X_K and F_K can be recovered from (18) and (19), respectively. Finally, we prove that for almost every compatible parameter K, the matrix X_K in (18) is non-singular.

We start proving the first point. Let K be a compatible input parameter matrix as in (12), and for each $i \in \{1, ..., v\}$ and $k \in \{1, ..., g_i\}$, let $X_{i,k}$, X_i and X_K be constructed as in (16)-(18) respectively. Then the column vectors of $X_{i,k}$ satisfy (13)-(15) by construction. Thus

$$U_{1}^{\top}(A - \lambda_{i}I_{n})x_{i,k}(1) = U_{1}^{\top}(A - \lambda_{i}I_{n})N_{i}K_{i,k}(1) = 0, (20)$$

$$U_{1}^{\top}(A - \lambda_{i}I_{n})x_{i,k}(2) = U_{1}^{\top}(A - \lambda_{i}I_{n})M_{i}U_{1}^{\top}x_{i,k}(1)$$

$$+U_{1}^{\top}(A - \lambda_{i}I_{n})N_{i}K_{i,k}(2)$$

$$= U_{1}^{\top}x_{i,k}(1)$$
(21)

:

$$U_{1}^{\top}(A - \lambda_{i}I_{n})x_{i,k}(p_{i,k}) = U_{1}^{\top}(A - \lambda_{i}I_{n})M_{i}U_{1}^{\top}x_{i,k}(p_{i,k} - 1) + U_{1}^{\top}(A - \lambda_{i}I_{n})N_{i}K_{i,k}(p_{i,k}) = U_{1}^{\top}x_{i,k}(p_{i,k} - 1).$$
(22)

Hence the vectors $x_{i,k}(1), \dots, x_{i,k}(p_{i,k})$ form a chain of generalised eigenvectors for the matrix $U_1^{\top}(A - \lambda_i I_n)$, and so

$$U_1^{\top} (A X_{i,k} - X_{i,k} J_k(\lambda_i)) = 0.$$
 (23)

Thus,

$$U_1^{\top} (AX_i - X_i J(\lambda_i)) = 0 \tag{24}$$

and finally we have

$$U_1^{\top} (AX_K - X_K \Lambda) = 0. \tag{25}$$

Assume X_K is non-singular and obtain F_K from (19). We note that F_K is a real matrix because for each odd $i \in \{1, ..., 2\sigma\}$, we have $\lambda_{i+1} = \overline{\lambda}_i$ and $X_{i+1} = \overline{X}_i$. Multiplying through by $B = U_0 Z$ we obtain

$$BF_K = X_K \Lambda X_K^{-1} - A \tag{26}$$

and hence X_K and F_K satisfy (2).

Next we show that the above parametrisation is exhaustive. We let X and F be any pair of matrices satisfying (2) such that the eigenstructure of A + BF is described by $(\mathcal{L}, \mathcal{M}, \mathcal{P})$. Then we can decompose X into block matrices

$$X = [X_1 | X_2 | \dots | X_V] \tag{27}$$

where for $i \in \{1, \dots, v\}$,

$$X_i = [X_{i,1} | X_{i,2} | \dots | X_{i,k}]$$
 (28)

and for $k \in \{1, \dots, g_i\}$

$$X_{i,k} = [x_{i,k}(1) | x_{i,k}(2) | \dots | x_{i,k}(p_{i,k})]$$
 (29)

and the vectors $x_{i,k}(1), x_{i,k}(2), \dots, x_{i,k}(p_{i,k}-1)$ form a chain of generalised eigenvectors for A+BF with respect to λ_i . Hence, we have

$$(A + BF - \lambda_i I_n) x_{i,k}(1) = 0 \tag{30}$$

$$(A + BF - \lambda_i I_n) x_{i,k}(2) = x_{i,k}(1)$$
 (31)

:

$$(A + BF - \lambda_i I_n) x_{i,k}(p_{i,k}) = x_{i,k}(p_{i,k} - 1)$$
 (32)

Thus from (30) we have

$$(A - \lambda_i I_n) x_{i,k}(1) = -BF x_{i,k}(1)$$

$$\Rightarrow U_1^{\top} (A - \lambda_i I_n) x_{i,k}(1) = -U_1^{\top} BF x_{i,k}(1) = 0$$
 (33)

as $U_1^{\top}B = 0$. Hence there exists a compatible parameter matrix $K_{i,k}(1)$ of dimension $m \times 1$ such that (13) holds. Also from (31) we have

$$(A - \lambda_{i}I_{n})x_{i,k}(2) = -BFx_{i,k}(2) + x_{i,k}(1)$$

$$\Rightarrow U_{1}^{\top}(A - \lambda_{i}I_{n})x_{i,k}(2) = -U_{1}^{\top}BFx_{i,k}(2) + U_{1}^{\top}x_{i,k}(1)$$

$$= U_{1}^{\top}x_{i,k}(1)$$

and hence (14) holds for some parameter matrix $K_{i,k}(2)$. Similarly we can use (32) to obtain the parameter $K_{i,k}(p_{i,k})$ such that (15) holds. Combining these parameters we obtain an $m \times p_{i,k}$ parameter matrix $K_{i,k}$; combining these for all $k \in \{1, \ldots, g_i\}$ we obtain a parameter matrix K_i of dimension $m \times m_i$, and finally combining these for all $i \in \{1, \ldots, v\}$ we obtain a parameter matrix K of dimension $m \times n$. Further it is clear that if λ_i and λ_{i+1} are such that $\overline{\lambda}_{i+1} = \lambda_i$ then $\overline{K}_{i+1} = K_i$. Hence applying the procedure in (13)-(15) with this parameter matrix K will yield $K_i = K_i$, and applying (19) with this $K_i = K_i$ yields $K_i = K_i$.

Finally let us prove the third point. We let $N_i \stackrel{\text{def}}{=} [n_{i,1} | \dots | n_{i,m}]$ be an orthonormal basis matrix for \mathcal{S}_i , and for each $i \in \{1,\dots,v\}$ and $k \in \{1,\dots,g_i\}$, we introduce vectors

$$v_{i,k}(1) = n_{i,k}$$

$$v_{i,k}(2) = M_i U_1^{\top} v_{i,k}(1)$$

$$\vdots$$

$$v_{i,k}(p_{i,k}) = M_i U_1^{\top} v_{i,k}(p_{i,k} - 1)$$
(34)

and using these we obtain matrices

$$V_{i,k} \stackrel{\text{def}}{=} [v_{i,k}(1) | v_{i,k}(2) | \dots | v_{i,k}(p_{i,k})], \tag{35}$$

$$V_i \stackrel{\text{def}}{=} [V_{i1} | V_{i2} | \dots | V_{i e_i}], \tag{36}$$

$$V \stackrel{\text{def}}{=} [V_1 \mid V_2 \mid \dots \mid V_V] \tag{37}$$

of dimensions $n \times p_{i,k}$, $n \times m_i$, and $n \times n$, respectively. Then we have $\operatorname{rank}(V) = n$, because if the rank is strictly smaller than n, then no parameter matrix K exists to construct F_K in (19) that will deliver the desired closed-loop eigenstructure. On the other hand, we showed that the parameterisation given by (19) is exhaustive and $(\mathcal{L}, \mathcal{M}, \mathcal{P})$ are an admissible Jordan structure. Hence, this means in particular that no feedback matrix can deliver the required closed-loop eigenstructure. This means that the pair (A, B) is not reachable, which leads to a contradiction.

Next let K be any compatible parameter matrix for $(\mathcal{L}, \mathcal{M}, \mathcal{P})$, let X = VK and assume X is singular, i.e. rank(X) < n-1. This means that one column of the matrix

$$[\nu_{1,1}(1)K_{1,1}(1)\dots\nu_{1,1}(p_{1,1})K_{1,1}(p_{1,1})\dots\\\dots\nu_{\nu,g_{\nu}}(1)K_{\nu,g_{\nu}}(1)\dots\nu_{\nu,g_{\nu}}(p_{\nu,g_{\nu}})K_{\nu,g_{\nu}}(p_{\nu,g_{\nu}})]$$

is linearly dependent upon the remaining ones. For the sake of argument, assume this is the last column. This means that there exist coefficients $\{\alpha_{i,k,l}: 1 \le i \le v, 1 \le k \le g_i, 1 \le l \le p_{i,k}\}$ (not all equal to zero) for which

$$\begin{array}{lll} v_{\nu,g_{\nu}}(p_{\nu,g_{\nu}})K_{\nu,g_{\nu}}(p_{\nu,g_{\nu}}) & = & \displaystyle\sum_{i=1}^{\nu-1}\sum_{k=1}^{g_{i}}\sum_{l=1}^{p_{i,k}} \,\alpha_{i,k,l}v_{i,g_{i}}(l) \\ & + \displaystyle\sum_{k=1}^{g_{\nu}-1}\sum_{l=1}^{p_{\nu,k}} \,\alpha_{\nu,k,l}v_{\nu,k}(l) \\ & + \displaystyle\sum_{l=1}^{p_{\nu,g_{\nu}}-1} \,\alpha_{\nu,g_{\nu},l}v_{\nu,g_{\nu}}(l). \end{array}$$

This implies that $\operatorname{rank}(VK) = n$ may fail only when $K_{V,g_V}(p_{V,g_V})$ lies on an (m-1)-dimensional hyperplane in the m-dimensional parameter space. Thus the set of compatible parameter matrices K that can lead to a loss of rank in X_K is given by the union of a finite number of hyperplanes of dimension at most m-1 within the parameter space. Since hyperplanes have measure zero with respect to Lebesgue measure on the m-dimensional parameter space, we conclude the set of parameter matrices K leading to singular X_K has zero Lebesgue measure.

III. MINIMUM GAIN POLE PLACEMENT

We utilise the parametric form introduced in the previous section to consider the problem of minimising the norm of the gain matrix F. More precisely, we consider the unconstrained optimisation problem

$$(\mathscr{P}): \quad \min_{K} \|F_K\|_{FRO}^2 \tag{38}$$

where F_K in (19) arises from any compatible parameter matrix K. Problem \mathscr{P} may be addressed via a gradient search employing the first and second order derivatives of $||F_K||^2_{FRO}$. From these the gradient and Hessian matrices are easily obtained, and unconstrained nonlinear optimisation methods can then be used to seek local minima. Such an optimisation approach was considered in [16], but only for \mathscr{L} with distinct eigenvalues. The method presented in this paper can accommodate any desired admissible eigenstructure.

IV. ILLUSTRATIVE EXAMPLES

In this section, we compare the algorithm presented in this paper with the methods given in [11], [14], [15].

Example 4.1: We consider Example 1 in [15], and seek to design a deadbeat controller, which can be achieved with one Jordan mini-block of dimension two, and two blocks of dimension 1. The method of [15] aims to minimise the Frobenius norm of the gain matrix and delivers the feedback matrix

$$F = -\begin{bmatrix} 0.5 & 0.5 & -0.0889 & 0.4556 \\ 0.5 & -0.5 & -0.1111 & -0.0556 \\ 0 & 0 & 0.2444 & 0.6222 \end{bmatrix},$$

yielding a normalised eigenvector matrix X with $\kappa_{FRO}(X) = 431.36$ and gain matrix $||F||_{FRO} = 1.2953$. Applying our method, we also obtain the matrix F.

Example 4.2: We consider the example 3.1 in [11] with n = 4 and m = 2. The method presented in this paper produces the feedback matrix

$$F = \left[\begin{array}{cccc} 2.0000 & 0.0000 & -0.0000 & -2.0000 \\ 0.0000 & -2.0000 & 2.0000 & -0.0000 \end{array} \right],$$

whose Frobenius norm is equal to 4. This result ties up with the method in [11].

Example 4.3: Now we study the example in [14] with n = 9 and m = 4 in which a gain matrix is sought to place all the closed-loop poles at $\lambda = -0.55$. In this example, the controllability indexes are $\{3,2,2,2\}$. Hence, a gain matrix F can be obtained such that $(A + BF - \lambda I)^l = 0$ for any l between 3 and 9.

In this example, the maximum iteration is chosen as 5000 and the initial condition is given as

$$K(0) = \operatorname{diag} \left\{ \begin{bmatrix} -1 \\ -2 \\ 0 \\ 2 \end{bmatrix}, \begin{bmatrix} 1 \\ -1 \\ 0 \\ 1 \end{bmatrix}, \begin{bmatrix} 1 \\ 0 \\ -1 \\ -1 \end{bmatrix}, \begin{bmatrix} 1 \\ -1 \\ 1 \\ 0 \end{bmatrix},$$

$$\begin{bmatrix} -1 \\ 3 \\ 2 \\ 0 \end{bmatrix}, \begin{bmatrix} 3 \\ 0 \\ -2 \\ 2 \end{bmatrix}, \begin{bmatrix} -4 \\ 1 \\ 0 \\ 2 \end{bmatrix}, \begin{bmatrix} 1 \\ 0 \\ 3 \\ -1 \end{bmatrix}, \begin{bmatrix} -2 \\ 1 \\ 1 \\ 2 \end{bmatrix} \right\}.$$

For the case $(A - \lambda I + BF)^3 = 0$, the method in [14] produces a feedback matrix F_1 with $||F_1||_{FRO} = 1.5 \times 10^7$. Our method based on the Klein-Moore parametric form in [11] produces a gain matrix F_2 with $||F_2||_{FRO} = 4.4 \times 10^5$.

The method given in this paper via the extended Kautsky-Nichols-van Dooren parametric form gives a gain matrix F_3 with $||F_3||_{FRO} = 1.3 \times 10^4$ where

$$F_3 = 10^4 * \begin{bmatrix} 0.1105 & -0.0004 & 0.0007 & 0.1075 \\ -1.2226 & -0.0008 & 0.0001 & 0.0096 \\ 0.0027 & 0.0680 & 0.0500 & -0.0032 \\ 0.0869 & -0.0004 & 0.0008 & 0.1322 \end{bmatrix}$$

For the case $(A - \lambda I + BF)^5 = 0$, the solution F_4 in [14] is such that $||F_4||_{\text{FRO}} = 9.2 \times 10^2$. The procedure in [11] results in a gain matrix F_5 with $||F_5||_{\text{FRO}} = 6.8 \times 10^2$. Using our scheme, we obtain a gain matrix F_6 with $||F_6||_{\text{FRO}} = 7.3 \times 10^2$ where

$$F_6 = \begin{bmatrix} 254.3428 & -2.3338 & 2.1648 & -247.0867 \\ -17.2078 & -76.7139 & 65.2416 & -3.3914 \\ -3.1697 & -124.2937 & 364.2689 & -0.1693 \\ 194.1004 & -3.8408 & 3.1736 & 152.1953 \end{bmatrix}$$

V. CONCLUSION

We have extended the classic pole placement method of Kautsky, Nichols and van Dooren to obtain a parametric form for the problem of exact pole placement that can accommodate any desired eigenstructure with arbitrary multiplicities. The method places no restrictions on the set of poles that can be assigned, nor their multiplicities, other than those implied by the constraints of the Rosenbrock theorem. The method provides an interesting parallel to the parametric formula given in [11] that also achieved arbitrary pole placement, but was derived from the Klein-Moore parametric form. Examples were given to show that this method delivers pole placement with considerably less matrix gain than the alternative in [14]. The comparisons against the method of [11] showed similar performance in minimising the matrix gain. Future work will consider whether either of these two optimal pole placement methods enjoys any significant performance advantages over the other, with respect to

VI. APPENDIX

Here we consider the first and second derivatives of f in (38). We define

$$\chi_i \stackrel{\text{def}}{=} \begin{cases}
\mathfrak{Re}\{K_i\} & i \in \{1, \dots, 2\sigma\} \text{ odd,} \\
\mathfrak{Im}\{K_{i-1}\} & i \in \{1, \dots, 2\sigma\} \text{ even,} \\
K_i & i \in \{2\sigma+1, \dots, \nu\}.
\end{cases}$$

minimising the matrix gain.

Let

$$H_K = \mathfrak{Re}\{X_K\}. \tag{39}$$

Define $\chi_{i,k}(l,r)$ as the r-th entry of $\chi_{i,k}(l)$. We compute the derivative of $Y_{p,q}$ with respect to $\chi_{i,k}$. We have

$$\frac{\partial H_{p,q}}{\partial \chi_{i,k}(l,r)} = 0$$

for $p \in \{1, ..., 2\sigma\}$ with $p \neq i, p \neq i + \sigma, p + \sigma \neq i$ and $p \in \{2\sigma + 1, ..., v\}$ with $p \neq i$. Define

$$P(i,l) \stackrel{\text{\tiny def}}{=} \left\{ egin{array}{ll} \{M_i U_1^{ op}\}^l N_i & ext{if } l \geq 0, \\ 0 & ext{otherwise.} \end{array}
ight.$$

For each $i \in \{1, ..., \sigma\}$, $k \in \{1, ..., g_i\}$, $h, l \in \{1, ..., p_{i,k}\}$ and $r \in \{1, ..., m\}$ we find

$$\begin{split} \frac{\partial H_{i,k}(h)}{\partial \chi_{i,k}(l,r)} &= \mathfrak{Re}\{P(i,h-l)\}(r),\\ \frac{\partial H_{i+\sigma,k}(h)}{\partial \chi_{i,k}(l,r)} &= \mathfrak{Im}\{P(i,h-l)\}(r),\\ \frac{\partial H_{i,k}(h)}{\partial \chi_{i+\sigma,k}(l,r)} &= -\mathfrak{Im}\{P(i,h-l)\}(r),\\ \frac{\partial H_{i+\sigma,k}(h)}{\partial \chi_{i+\sigma,k}(l,r)} &= \mathfrak{Re}\{P(i,h-l)\}(r). \end{split}$$

For each $i \in \{2\sigma + 1,...,v\}, k \in \{1,...,g_i\}, h,l \in \{1,...,p_{i,k}\}$ and $r \in \{1,...,m\}$ we have

$$\frac{\partial H_{i,k}(h)}{\partial \chi_{i,k}(l,r)} = P(i,h-l)(r).$$

Let $Y_K = H_K^{-1}$. Using the well-known formula $\frac{\partial Y_K}{\partial \chi_{l,k}(l,r)} = -Y_K \frac{\partial H_K}{\partial \chi_{l,k}(l,r)} Y_K$, we compute the first and second derivatives of $\|F_K\|_{\text{PRO}}^2$ as

$$\frac{\partial \|F_K\|_{\text{FRO}}^2}{\partial \chi_{i,k}(l,r)} = 2 \operatorname{trace} \left(F_K^\top Q_K(i,k,l,r) \right)$$

and

$$\begin{split} & \frac{\partial^{2} \|F_{K}\|_{\text{FRO}}^{2}}{\partial \chi_{i_{1},k_{1}}(l_{1},r_{1})\partial \chi_{i_{2},k_{2}}(l_{2},r_{2})} \\ &= 2 \operatorname{trace} \left(Q_{K}(i_{2},k_{2},l_{2},r_{2})^{\top} Q_{K}(i_{1},k_{1},l_{1},r_{1}) \right. \\ & \left. - F_{K}^{\top} Q_{K}(i_{2},k_{2},l_{2},r_{2}) \frac{\partial H_{K}}{\partial \chi_{i_{1},k_{1}}(l_{1},r_{1})} Y_{K} \right. \\ & \left. - F_{K}^{\top} Q_{K}(i_{1},k_{1},l_{1},r_{1}) \frac{\partial H_{K}}{\partial \chi_{i_{2},k_{2}}(l_{2},r_{2})} Y_{K} \right), \end{split}$$

where

$$\begin{split} Q_K(i,k,l,r) &= \\ Z^{-1}U_0^\top \Big(\frac{\partial H_K}{\partial K_{i,k}(l,r)} \Lambda Y_K - H_K \Lambda Y_K \frac{\partial H_K}{\partial K_{i,k}(l,r)} Y_K \Big). \end{split}$$

REFERENCES

- [1] J. Kautsky, J. N.K. Nichols and P. Van Dooren, Robust Pole Assignment in Linear State Feedback, *International Journal of Control*, vol. 41, pp. 1129–1155, 1985.
- [2] H. H. Rosenbrock, State-Space and Multioariable Theory. New York: Wiley, 1970.
- [3] R. Byers and S. G. Nash, Approaches to robust pole assignment, International Journal of Control, vol. 49, pp. 97-117, 1989.

- [4] S.P. Bhattacharyya and E. de Souza, Pole assignment via Sylvester's equation, *Systems & Control Letters*, vol. 1(4), pp. 261–263, 1982.
- [5] M.M. Fahmy and J. O'Reilly, Eigenstructure Assignment in Linear Multivariable Systems-A Parametric Solution, *IEEE Transactions on Automatic Control*, vol. 28, pp. 990–994, 1983.
- [6] E. Chu, Pole assignment via the Schur form, Systems & Control Letters vol. 56, pp, 303-314, 2007.
- [7] M. Ait Rami, S.E. Faiz, and A. Benzaouia, Robust Exact Pole Placement via an LMI-Based Algorithm, *IEEE Transactions on Automatic Control*, Vol. 54(2) pp. 394–398, 2009.
- [8] R. Schmid, T. Nguyen and A. Pandey, Optimal Pole placement with Moore's algorithm, in *Proceedings 1st IEEE Australian Control* Conference, Melbourne, Australia, 2011.
- [9] R. Schmid, A. Pandey and T. Nguyen, Robust Pole placement with Moore's algorithm, *IEEE Transactions on Automatic Control* vol. 59, pp. 500–505, 2014.
- [10] B.C. Moore, On the Flexibility Offered by State Feedback in Multivariable systems Beyond Closed Loop Eigenvalue Assignment, *IEEE Transactions on Automatic Control*, vol. 21(5), pp. 689–692, 1976.
- [11] R. Schmid, L. Ntogramatzidis, T. Nguyen and A. Pandey, Arbitrary pole placement with minimum gain, *Proceedings 21st Mediterranean Conference on Control and Automation*, Crete, 2013.
- [12] R. Schmid, L. Ntogramatzidis, T. Nguyen and A. Pandey, Robust repeated pole placement, to appear *Proceedings 3rd IEEE Australian Control Conference*, Perth, 2013.
- [13] G. Klein and B.C. Moore, Eigenvalue-Generalized Eigenvector Assignment with State Feedback, *IEEE Transactions on Automatic Control*, vol. 22(1), pp. 141–142, 1977.
- [14] A. Linnemann, An algorithm to compute state feedback matrices for multi-input deadbeat control, *Systems & Control Letters* vol. 25, pp, 99-102, 1995.
- [15] M. Ataei and A. Enshaee, Eigenvalue assignment by minimal state-feedback gain in LTI multivariable systems, *International Journal of Control*, vol. 84, pp. 1956-1964, 2011.
- [16] H.K. Tam and J. Lam, Newton's approach to gain-controlled robust pole placement, *IEE Proc.-Control Theory Applications*. 144(5), pp. 439–446, 1997.