



Use of Three-Dimensional Printing in Modelling an Anatomical Structure with a High Computed Tomography Attenuation Value: A Feasibility Study

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Introduction: Three-dimensional (3D) printing provides an opportunity to develop anthropomorphic computed tomography (CT) phantoms with anatomical and radiological features mimicking a range of patients' conditions, thus allowing development of individualised, low dose scanning protocols. However, previous studies of 3D printing in CT phantom development could only create anatomical structures using potassium iodide with attenuation values up to 1200 HU which is insufficient to mimic the radiological features of some high attenuation structures such as cortical bone. This study aimed at investigating the feasibility of using 3D printing in modelling cortical bone with a non-iodinated material. **Methods:** This study had 2 stages. Stage 1 involved a vat photopolymerisation 3D printer to directly print cube phantoms with different percentage compositions of calcium phosphate (CP) and resin (approach 1), and approach 2 using a material extrusion 3D printer to develop a cube mould for infilling of the CP with hardener as the phantom. The approach able to create the cube phantom with the CT attenuation value close to that of a tibial mid-diaphysis cortex of a real patient, 1475 ± 205 HU was employed to develop a tibial mid-diaphysis phantom. The mean CT numbers of the cube and tibia phantoms were measured and compared with that of the original CT dataset through unpaired *t*-test. **Results:** All phantoms were scanned by CT using a lower extremity scanning protocol. The moulding approach was selected to develop the tibia mid-diaphysis phantom with CT attenuation value, 1434 ± 184 HU which was not statistically significantly different from the one of the original dataset ($p = 0.721$). **Conclusion:** This study demonstrates the feasibility to use the material extrusion 3D printer to create a tibial mid-diaphysis mould for infilling of the CP as an anthropomorphic CT phantom and the attenuation value of its cortex matches the real patient's one.

Keywords: Calcium Phosphate, Computed Tomography, Hounsfield Unit, Mould, Phantom, Three-Dimensional Printing.

1. INTRODUCTION

Use of three-dimensional (3D) printing in medicine has become popular for some years [1]. Examples of its applications include development of personalised medical devices and anatomical models for surgical planning, teaching and research [1–7]. Recently, studies have shown the use of 3D printing in anthropomorphic phantom development for quality assurance of medical radiation sciences procedures such as intensity modulated radiation therapy [8, 9], stereotactic body radiation therapy [10], paediatric radiography [11], digital tomosynthesis [12–14] and computed tomography (CT) [2, 15–18]. Among those studies, the

CT phantom development appears to be the more common 3D printing research area.

The CT is the greatest contributor to collective medical radiation dose. However, CT scanning protocols of many institutions are not optimised as per patients' characteristics to address its radiation dose burden [19, 20]. Commercial phantoms have been used for CT scanning protocol optimisation for decades [18]. Despite their high cost, they only mimic features of standard-sized patients which appear not suitable for testing customised scanning protocols for various patients' characteristics, e.g., individual patients' sizes, pathological conditions, etc. Their use for the CT dose optimisation tends to be limited [2, 4, 17, 18]. Nonetheless, the 3D printing provides an opportunity to develop the CT phantoms with anatomical and radiological features

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mimicking a range of patients' conditions which allow development of individualised, low dose protocols to suit different clinical tasks without sacrificing diagnostic quality [16–18]. Also, their development process requires shorter time with lower cost when compared to the commercial phantoms [3, 17, 18].

The technologies for 3D printing in medicine include vat photopolymerisation (stereolithography [SLA]/digital light processing [DLP]), material jetting (PolyJet/multi-jet modelling [MJM]), binder jetting, material extrusion (fused deposition modelling [FDM]), powder bed fusion (selective laser sintering [SLS]/direct metal laser sintering [DMLS]/selective laser melting [SLM]/electron beam melting [EBM]), sheet lamination and directed energy deposition. Their details including advantages and limitations have been published elsewhere [5, 21], and only the key issues related to the CT phantom development are discussed in this paper.

The previous CT phantom development studies reported uses of the material jetting to construct lung [16], liver and brain phantoms [17], the material extrusion to build a cardiac model [2], and the sheet lamination to produce abdomen [18], head and neck phantoms [15]. Those studies claimed their CT phantoms had shapes and attenuation values measured in Hounsfield unit (HU)/CT numbers similar to corresponding anatomical structures. However, apparently, their phantom evaluation just covered the CT attenuation value measurement because the aim of their phantom development was for CT scanning protocol optimisation rather than surgical planning which requires a close resemblance of shape [2, 15–18]. It is noted that the traditional 3D printing materials such as photopolymers can only produce models with CT numbers about 20–130 HU and are unable to make bone-mimicking structures. In order to produce structures with high attenuation values, substances such as iodine, barium, calcium and bismuth can be mixed with the traditional materials for 3D printing [16, 17]. Another strategy is to use the traditional resins to make a 3D printed container/mould resembling an anatomical structure with infill of the high attenuation materials to form a phantom. The mould could be removed after infilling if required [17]. The former approach was used by Jahnke et al. [18] to radiopaquely print stacks of CT images using mixtures of standard inkjet ink and potassium iodide on paper for creating the CT phantoms via the sheet lamination method. Their phantoms had attenuation values up to 1200 HU. The latter approach was successfully implemented by Abdullah et al. [2] to produce the cardiac phantom with hollow regions for filling air (−894.1 HU), oil (−92.4 HU), jelly (25.9 HU) and iodinated contrast medium (354.3 HU).

The potassium iodide appears as a promising material to create individualised CT phantoms of high attenuation structures with CT numbers up to 1200 HU [2, 18]. However, the other materials for this purpose suggested in the literature seem not tested yet [17]. The common high attenuation structure in human body is cortical bone with CT numbers ranging between 500 HU and 2000 HU [22, 23]. To fully realise the use of 3D printing in development of customised CT whole body phantom which has structures with attenuation values ranging between −1000 HU and 2000 HU for CT scanning protocol optimisation, future studies should focus on cortical bone model development as this remains a challenging area [16, 22]. The aim of this study was to investigate the feasibility of using 3D printing in modelling the cortical bone with a non-iodinated material.

2. METHODS

This study's design was similar to the other 3D printing study in the CT phantom development which had two stages [18]. Stage 1 involved creation of 2 cm³ cube phantoms with various attenuation properties to identify appropriate arrangements for stage 2 to develop a CT anthropomorphic phantom. The aforementioned two approaches for making high attenuation structures were implemented in stage 1 [17]. The anthropomorphic phantom developed in stage 2 was a model of a right tibial mid-diaphysis of a 70-year-old male patient who underwent a CT scan (without any remarkable abnormality). The tibial mid-diaphysis was chosen for the phantom development because it has high cortical to trabecular bone ratio and simple geometry suitable for this study [24, 25]. A free, open source 3D visualisation program, 3DSlicer 4.8.1 (The Slicer Community, MA, USA) was used with its 'draw a 3D cube' tool to make the 3D cube mesh model, and for image post-processing and segmentation of anonymised digital imaging and communications in medicine (DICOM) CT images of the patient to make the tibia and fibula mesh model based on the segmented volume data. The mesh models were saved in standard tessellation language (STL) format for 3D printing [2, 7–9, 21]. Institutional review board approval was waived because of the use of the anonymised CT images. The high attenuation material selected for the phantom development was calcium phosphate (CP) monobasic monohydrate ($\text{Ca}(\text{H}_2\text{PO}_4)_2 \cdot \text{H}_2\text{O}$) as the CP is the major component of the cortical bone [26].

2.1. Stage 1-Cube Phantom Development

For the first approach, a vat photopolymerisation 3D printer (Kudo3D Titan 1, Kudo3D Inc., CA, USA) was used with mixtures of photocurable liquid resin (Monocure 3D Photoreactive Clear Resin, Monocure Pty Ltd., NSW, Australia) and the ring milled CP to create the cube phantoms with different percentage compositions of these two materials [5, 17]. The vat photopolymerisation 3D printer is commonly used to directly print bone models because it can produce models with fine details [5, 27]. Ring milling of the CP was to reduce its particle size for facilitating the mixing process [28].

Similar to Abdullah et al.'s study [2], a material extrusion 3D printer (Axiom 20, Airwolf 3D, CA, USA) was employed to implement the second approach by creating a cube container (mould) using NinjaFlex 3D printing material (Fenner Inc., PA, USA) for infilling of a 2 cm³ volume of CP and epoxy resin (hardener) mixture. The main advantage of the material extrusion 3D printer is its low cost [5, 27]. The mixture was prepared by gradually adding the epoxy resin and its hardener to the CP with stirring until becoming a paste. After the mixture hardened (48 h), the mould was cut out to form the cube phantom [29]. Figure 1 summarises the steps of approaches 1 and 2.

2.2. Stage 2-Tibial Mid-Diaphysis Phantom Development

The approach able to create the cube phantom with the CT attenuation value close to that of the right tibial mid-diaphysis cortex of the original CT dataset, 1475 ± 205 HU (measured over 6 consecutive axial images) was employed to create the right tibial mid-diaphysis phantom [15]. A free, open source mesh processing program, MeshLab 2016.12 (Istituto di Scienza e Tecnologie dell'Informazione, Pisa PI, Italy) was used to refine the mesh

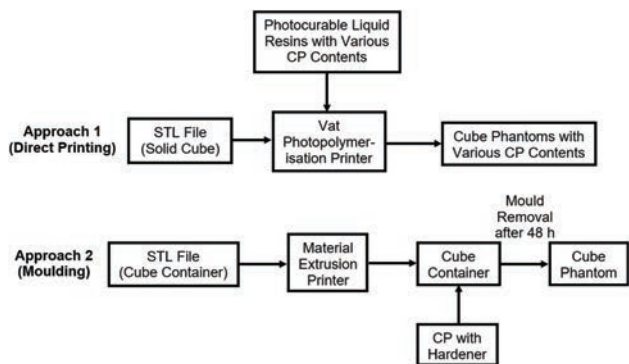


Fig. 1. Summary of the steps involved in approaches 1 and 2 of stage 1. CP, calcium phosphate; STL, standard tessellation language.

model generated by the 3DSlicer 4.8.1 program prior to the 3D printing [30].

2.3. Evaluation of CT Attenuation Property of Phantoms

Both the cube and tibial mid-diaphysis phantoms were scanned on a 128-slice CT scanner (SOMATOM Definition AS+, Siemens Medical Solutions, PA, USA) with following scanning parameters, 100 kV, 100 mA, 2 mm slice thickness and 0.8 pitch similar to those used for the original lower extremity CT dataset acquisition. The acquired DICOM CT images of the phantoms were exported to a workstation with a free, open source image processing program, ImageJ 1.47 (National Institutes of Health, MD, USA) for measuring average CT attenuation values of regions of interest (the cube and the tibial mid-diaphysis cortex) over a volume of 6 consecutive axial images [15]. An unpaired *t*-test was used to compare the average CT attenuation value of each phantom with that of the right tibial mid-diaphysis cortex of the original CT dataset. GraphPad InStat 3.06 (GraphPad Software Inc, CA, USA) was used for the statistical analysis. A *p*-value less than 0.05 obtained from the *t*-test was considered statistically significant difference.

Table I. The computed tomography (CT) attenuation values of the cube phantoms.

Cube (composition)	CT attenuation value (Mean ± SD)	<i>P</i> -value*
A (100% of photocurable liquid)	109 ± 20 HU	<0.0001
B (90% of photocurable liquid with 10% of CP)	179 ± 47 HU	<0.0001
C (80% of photocurable liquid with 20% of CP)	195 ± 82 HU	<0.0001
D (70% of photocurable liquid with 30% of CP)	474 ± 105 HU	<0.0001
E (CP with hardener)	1493 ± 72 HU	0.8459

Notes: CP, calcium phosphate; HU, Hounsfield unit; SD, standard deviation. **P*-value of unpaired *t*-test for comparing the mean CT attenuation value of each phantom with that of the tibial mid-diaphysis cortex of the original CT dataset, 1475 ± 205 HU.

3. RESULTS

3.1. Stage 1-Cube Phantom Development

Figure 2 illustrates the cube phantoms developed by using the approach 1-direct printing (cubes A–D) and the approach 2-moulding (cube E), and their corresponding axial CT images. An irregular contour is noted in the cube D images because of excessive CP within the resin (70% of photocurable liquid with 30% of CP) causing it unable to become a proper colloidal suspension for the vat photopolymerisation 3D printing. Resins with the CP content greater than 30% were not prepared and tested further. The cube E was created through putting the CP with hardener into the cube mould printed by the material extrusion 3D printer. The cube E appears not accurately resembling the shape of a cube. Table I shows the CT attenuation values of these cube phantoms. Only the CT attenuation value of the cube E matches the one of the tibial mid-diaphysis cortex of the original CT dataset. The moulding approach was used in stage 2 for the tibial mid-diaphysis phantom development.

3.2. Stage 2-Tibial Mid-Diaphysis Phantom Development

Figure 3 illustrates the mould printed by the material extrusion 3D printer and infilling of the CP with hardener to create the

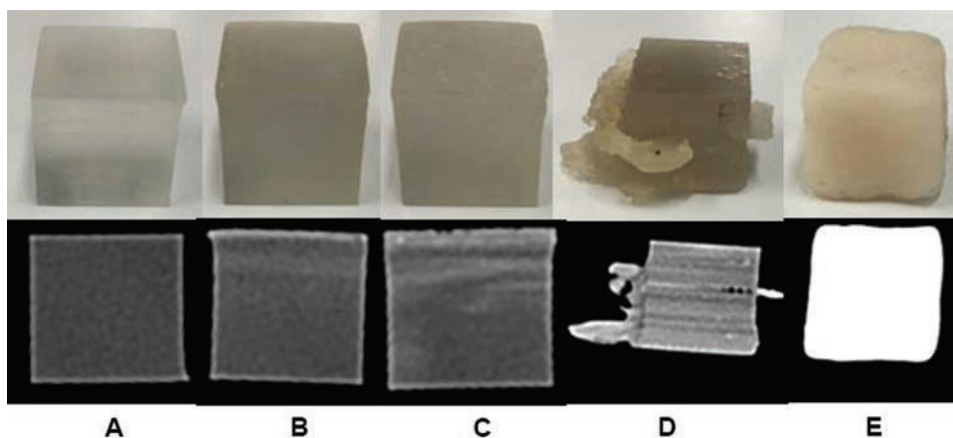


Fig. 2. The cube phantoms developed with the use of the approach 1-direct printing (cubes A–D) and the approach 2-moulding (cube E), and their corresponding axial computed tomography images. The resin compositions of the cubes A–D were 100% of photocurable liquid, 90% of photocurable liquid with 10% of calcium phosphate (CP), 80% of photocurable liquid with 20% of CP, and 70% of photocurable liquid with 30% of CP respectively.

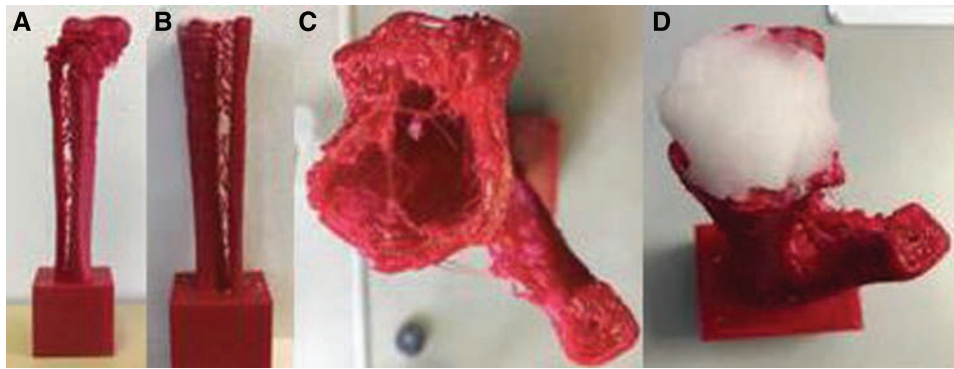


Fig. 3. The tibial mid-diaphysis phantom development process. (A) The mould was printed. (B and C) The mould with its proximal (top) part removed for infilling of the CP with hardener. (D) The mould with the infill of the CP.

tibial mid-diaphysis phantom. The mould printing time was about 6 h, and the phantom hardening and mould removal process required 48 h. The cost of the NinjaFlex 3D printing material and the CP were about US\$14 and US\$50 respectively. Figure 4 shows the tibial mid-diaphysis phantom and the original CT images. The phantom resembled the features of the tibial mid-diaphysis to some extent. For example, its anterior crest was illustrated. However, the contour of the phantom was not smooth. The CT attenuation value of the phantom was 1434 ± 184 HU which was not statistically significantly different from that of the original dataset ($p = 0.721$).

4. DISCUSSION

This study shows the material extrusion 3D printer could be used to create the tibial diaphysis mould for infilling of the CP and hardener mixture to develop the CT phantom of the cortical bone of the tibial mid-diaphysis with its attenuation value similar to that of the real patient, 1475 ± 205 HU. The highest attenuation value that could be achieved in the previous study of 3D printing in CT phantom development was 1200 HU. The potassium iodide was used as part of its 3D printing material [18]. Apparently, the use of potassium iodide may not be adequate to create some high attenuation anatomical structures but this is required for building a customised CT whole body phantom with the CT numbers of structures ranging between -1000 HU and 2000 HU [16]. The CP could be utilised for developing these high attenuation structures.

The tibial mid-diaphysis phantom development time and cost of this study were comparable to the other similar study which were shorter and less expensive than those of the commercial phantom [2]. Although the general shape of the phantom appears similar to the original one, some external contour defects are also found (Fig. 4). As the NinjaFlex 3D printing material is not transparent, it was difficult to ensure the CP and hardener mixture filling up the mould completely causing the contour defects eventually. This issue was also reported in a study using a 3D printed mould to develop a kidney phantom. Use of transparent printing materials such as VeroClear and TangoPlus (Stratasys Ltd., MN, USA) with a material jetting printer was recommended. The TangoPlus is better for the mould creation because of its flexibility leading to ease of the mould removal [31]. However, these printing materials are relatively expensive [5].

The tibia mid-diaphysis phantom developed in this study also had another issue which was not a hollow structure. As noted in that kidney phantom development study, an outer and an inner moulds should be prepared for creating a phantom with a hollow space. Alignment of the 2 moulds involved in that approach might be challenging and their misalignment could affect geometrical accuracy of the phantom [31]. However, unlike the models for surgical planning, the anthropomorphic CT phantoms do not require high geometrical accuracy normally [2, 15–18]. The tibia mid-diaphysis phantom created in this study should serve its purpose to some extent.

The tibial mid-diaphysis was selected for the phantom development in this feasibility study because of its simple geometry [25].

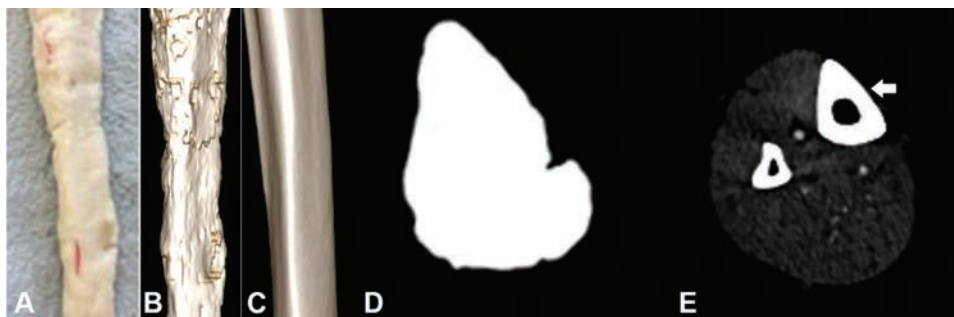


Fig. 4. The tibial mid-diaphysis phantom and original computed tomography (CT) images. (A) The photograph of the phantom. (B) The surface rendered CT image of the phantom. (C) The surface rendered CT image of the tibial mid-diaphysis of the original dataset. (D) The axial CT image of the phantom. (E) The axial CT image of the original dataset showing the tibial mid-diaphysis (arrow).

Nevertheless, this phantom developed by the moulding approach still had a number of geometrical defects. It is noted in Figure 2 that the direct printing approach would be better to create phantoms with higher geometrical accuracy which is important for modelling complex anatomical structures such as molar teeth. A previous study demonstrated feasibility of mixing 15% of CP nanoparticles with 85% of thermoplastics for the material extrusion 3D printer to directly print a molar tooth model. However, its CT attenuation value was not assessed, thus unable to determine whether it was comparable to a real tooth's attenuation value [32]. This study shows that it was not feasible to use the vat photopolymerisation printer to directly print a cube phantom with high (30% of) CP content. Nonetheless, it remains unclear whether models with CP content greater than 30% can be directly printed by the material extrusion and/or vat photopolymerisation printers when the CP nanoparticles are used. It is because CP particle size affects printability of the 3D printing materials [28].

This study has several limitations. Only two types of 3D printers (vat photopolymerisation and material extrusion) and one high attenuation material (CP monobasic monohydrate) were involved in this study. However, most of the previous studies of 3D printing in the CT phantom development just used one single printer [2, 16–18]. Furthermore, it is not uncommon to investigate only one high attenuation material for the phantom creation [15, 18]. The geometrical accuracy of the cube and tibial mid-diaphysis phantoms was not quantitatively assessed and the inner mould was not printed for creating a hollow tibial mid-diaphysis phantom. Nonetheless, high geometrical accuracy is normally not required for the anthropomorphic CT phantoms and hence this was not quantitatively evaluated in the previous studies either [2, 15–18]. For future research, more types of 3D printers [5, 21] and a wide range of high attenuation materials such as barium and bismuth [17] with different sizes including nanoparticles [32] as part of the printing materials should be investigated for developing phantoms with high attenuation structures. Apart from assessment of their CT attenuation properties, their geometrical accuracy should also be quantitatively assessed.

5. CONCLUSION

A tibial mid-diaphysis CT phantom with its attenuation value of the cortex (1434 ± 184 HU) matching the real patient's one (1475 ± 205 HU) was developed by the moulding approach with the use of the material extrusion 3D printer and the CP. The attenuation value of this phantom is greater than the highest attenuation value (1200 HU) achieved in the previous study of 3D printing in the CT phantom development with the use of potassium iodide as part of the printing material. The CP seems to be a better choice to create the high attenuation structures such as the cortical bone for developing a customised CT whole body phantom.

The general shape of the tibial mid-diaphysis phantom appears similar to that of the original dataset. However, it had some external contour defects and was not a hollow structure. The direct printing approach would be better to create the phantoms with higher geometrical accuracy but mixing the high attenuation matter with the traditional printing materials to directly print the anatomical structures with high attenuation values remains a technical challenge which needs to be resolved. The use of the CP nanoparticles as the high attenuation material might address this issue.

Conflicts of interest

There are no conflicts to declare.

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